

ALLOY 200/201 DATA SHEET

UNS N02200 / UNS N02201

GENERAL PROPERTIES

//// Alloy 200 (UNS designation N02200) and Alloy 201 (UNS designation N02201) are wrought commercially pure nickel. The alloys differ only in the maximum carbon level allowed by specification, 0.15 % maximum for Alloy 200 and 0.02 % maximum for Alloy 201. Both alloys provide highly ductile mechanical properties over a wide temperature range. Both alloys provide corrosion resistance in neutral to moderately reducing environments. In the annealed condition, either alloy possesses the approximate strength of mild steel. As-rolled material is sometimes furnished to provide higher strength levels.

//// Alloy 200 and Alloy 201 provide high thermal and electrical conductivity in comparison to nickel base alloys, stainless steels and low alloy steels. The alloys are ferromagnetic.

//// Because long-time exposures of Alloy 200 in the 800 to 1200 °F (427-649 °C) range result in precipitation of a carbon phase and loss of ductility, it is not recommended for service above 600 °F (316 °C). For applications above 600 °F (316 °C), the low carbon Alloy 201 should be considered.

//// For proposed service temperatures approaching 800 °F (427 °C), resistance to creep should be considered as a design factor.

APPLICATIONS

//// INDUSTRIES

- //// Food production;
- //// Fluorine generation;
- //// Storing and transportation of phenol;
- //// Manufacture and handling of sodium hydroxide;
- //// Production of hydrochloric acid and chlorination of hydro-carbons such as benzene, methane and ethane;
- //// Manufacture of vinyl chloride monomer;

//// FABRICATIONS

- //// Heat exchangers;
- //// Tube sheets;
- //// Piping;
- //// Shell plate;
- //// Tank heads;
- //// Tanks;
- //// Storage vessels;
- //// Mixers;
- //// Valves.



ALLOY 200 / 201

STANDARDS

| Product form | Specifications | | | | | |
|-----------------------|----------------|-------------|-----------------------|-------|-------|------|
| | ASTM | ASME | AMS | DIN | VdTÜV | UK |
| Plate sheet and Strip | B162 | SB162 | 5553 (N02201 only) | 17750 | 345 | 3072 |
| Rod and Bar | B160 | SB160 | – | 17752 | 345 | 3076 |
| Smls Pipe and tubind | B161/B163 | SB161/SB163 | – | 17751 | 345 | 3074 |

CHEMICAL COMPOSITION (%)

| Alloy | C | Mn | S | Si | Cu | Ni+Co | Fe |
|-------|----------|----------|----------|----------|----------|-----------|----------|
| 200 | 0.15 max | 0.35 max | 0.01 max | 0.35 max | 0.25 max | 99.00 min | 0.40 max |
| 201 | 0.02 max | 0.35 max | 0.01 max | 0.35 max | 0.25 max | 99.00 min | 0.40 max |

MECHANICAL PROPERTIES

//// SHORT TIME TENSILE PROPERTIES AS A FUNCTION OF TEMPERATURE

//// The following tables illustrate the short time room and elevated temperature tensile properties of annealed Alloy 200 and Alloy 201. The tables indicate that Alloy 200 is stronger than Alloy 201 in the annealed condition. Specifications generally recognize this difference by assigning lower minimum yield and tensile strength values to Alloy 201 than to Alloy 200.

//// ALLOY 200

| Temperature | | Yield Strength 0.2 % Offset | | | | Elongation |
|-------------|-----|-----------------------------|-----|--------|-----|------------|
| °F | °C | psi | MPa | psi | MPa | % in 2" |
| 68 | 20 | 21 500 | 148 | 67 000 | 462 | 47 |
| 200 | 93 | 21 000 | 145 | 66 500 | 458 | 46 |
| 400 | 204 | 20 200 | 139 | 66 500 | 458 | 44 |
| 600 | 316 | 20 200 | 139 | 66 200 | 456 | 47 |

//// ALLOY 201

| Temperature | | Yield Strength 0.2 % Offset | | | | Elongation |
|-------------|-----|-----------------------------|-----|--------|-----|------------|
| °F | °C | psi | MPa | psi | MPa | % in 2" |
| 68 | 20 | 15 000 | 103 | 58 500 | 403 | 50 |
| 200 | 93 | 15 000 | 103 | 56 100 | 387 | 45 |
| 400 | 204 | 14 800 | 102 | 54 000 | 372 | 44 |
| 600 | 316 | 14 300 | 98 | 52 500 | 362 | 42 |
| 800 | 427 | 13 500 | 93 | 41 200 | 284 | 58 |



ALLOY 200 / 201

////THE EFFECTS OF COLD WORKING

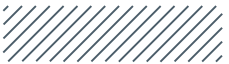
////The tensile properties of both Alloy 200 and Alloy 201 can be significantly enhanced by cold working. In plate products, this can be achieved by control of the finishing temperature in hot rolling and the elimination of the anneal that follows hot rolling. Sheet and strip can be cold rolled to higher strength. The typical range of enhancement of room temperature properties is shown in the next table. These properties depend on the thermomechanical history and section size and cannot be developed in all gages

////TYPICAL PROPERTY RANGES IN COLD WORKED ALLOY 200

| Form | Tensile Strength | | Yield Strength 0.2 % Offset | | Elongation % in 2" | Hardness | |
|-----------------------|------------------|---------|-----------------------------|---------|-----------------------|--------------------|------------|
| | ksi | MPa | ksi | MPa | | Birrell (3 000 kg) | Rockwell B |
| Rod and Bar | | | | | | | |
| Hot Fin | 60-85 | 415-585 | 15-45 | 105-310 | 55-35 | 90-150 | 45-80 |
| Cold drawn | 65-110 | 450-760 | 40-100 | 275-690 | 35-10 | 140-230 | 75-98 |
| CD or HR Ann | 55-75 | 380-520 | 15-30 | 105-210 | 55-40 | 90-120 | 45-70 |
| Plate | | | | | | | |
| Hot Rolled | 55-100 | 380-690 | 20-80 | 140-550 | 55-35 | 100-150 | 55-80 |
| HR Ann | 55-80 | 380-550 | 15-40 | 105-275 | 60-40 | 90-140 | 45-75 |
| Sheet | | | | | | | |
| Cold Rolled | 90-115 | 620-795 | 70-105 | 480-725 | 15-2 | - | 90 min |
| CR Ann | 55-75 | 380-520 | 15-30 | 105-210 | 55-40 | - | 70 max |
| Tube | | | | | | | |
| Stress Rel | 65-110 | 450-760 | 40-90 | 275-620 | 35-15 | - | 75-98 |
| Annealed | 55-75 | 380-520 | 12-30 | 85-210 | 60-40 | - | 70 max |
| Condenser Tube | | | | | | | |
| Annealed | 55-75 | 380-520 | 15-30 | 105-210 | 60-40 | - | 65 max |
| Stress Rel | 65-110 | 450-760 | 40-90 | 275-620 | 35-20 | - | 75-98 |

////TYPICAL PROPERTY RANGES IN COLD WORKED ALLOY 200

| Form | Tensile Strength | | Yield Strength 0.2 % Offset | | Elongation % in 2" | Hardness | |
|--------------------|------------------|---------|-----------------------------|---------|-----------------------|--------------------|------------|
| | ksi | MPa | ksi | MPa | | Birrell (3 000 kg) | Rockwell B |
| Rod and Bar | | | | | | | |
| HF, HF Ann | 50-60 | 345-415 | 10-25 | 70-170 | 60-40 | 75-100 | - |
| Cold drawn | 60-100 | 415-690 | 35-90 | 240-620 | 35-10 | 125-200 | - |
| CD Ann | 50-60 | 345-416 | 10-25 | 70-170 | 60-40 | 75-100 | - |
| Plate | | | | | | | |
| Hot Rolled | 50-70 | 345-485 | 12-35 | 83-240 | 60-35 | - | - |
| HR Ann | 50-70 | 345-485 | 12-35 | 83-240 | 60-40 | - | - |
| Tube, Pipe | | | | | | | |
| CD Ann | 50-70 | 345-485 | 10-28 | 70-195 | 60-40 | - | 62 max |
| Stress Rel | 60-105 | 415-725 | 30-85 | 205-585 | 35-15 | - | 75-98 |



ALLOY 200 / 201

////IMPACT STRENGTH

//// As measured by Charpy impact tests, Alloy 200 is one of the toughest metals. Both hot rolled and annealed samples have higher impact strength than cold-worked material.

////IMPACT PROPERTIES FOR ALLOY 200

| Condition | Hardness Birnell (3 000 kg) | Charpy-V | | Charpy Torsion | | | Charpy Tension | | Elong. in 3.54 in. (89.9 mm), % | Reduction of area (%) |
|--|-----------------------------------|----------|-----|----------------|----|--------|----------------|-----|---------------------------------------|--------------------------|
| | | Ft-lb | J | ft-lb | J | Twist* | Ft-lb | J | | |
| Hot Rolled | 107 | 200 | 271 | 29 | 39 | 103.5 | 98 | 132 | 20 | 83.1 |
| Cold Drawn-24 % reduction, stress-relieved | 177 | 204 | 277 | 35 | 47 | 102 | 88 | 119 | 19.5 | 71.2 |
| Cold Drawn-Annealed at 1350 °F (732 °C)/3 hrs | 109 | 228 | 309 | 29 | 39 | 103 | 113 | 153 | 33 | 75.1 |

////TYPICAL PROPERTY RANGES IN COLD WORKED ALLOY 200

| Condition | Temperature | | Tensile Strength | | Yield Strength 0.2 % Offset | | Elongation | Reduction | Hardness |
|------------|-------------|------|------------------|-----|-----------------------------|-----|------------|-------------|------------|
| | °F | °C | ksi | MPa | ksi | MPa | % in 2" | of Area (%) | Rockwell C |
| Hot Rolled | -310 | -190 | 103 | 710 | - | - | 51 | - | - |
| | -292 | -180 | 98 | 676 | 28 | 193 | - | - | - |
| | -112 | -80 | 76.4 | 527 | 27.5 | 190 | - | - | - |
| | room | room | 65.6 | 452 | 24.6 | 169 | 50 | - | - |
| Cold Drawn | -110 | -79 | 112.3 | 774 | 101.8 | 702 | 21.5 | 60.9 | 22 |
| | room | room | 103.4 | 713 | 97.4 | 672 | 16.3 | 66.9 | 19 |

PHYSICAL PROPERTIES //////////////////////////////////////

| | | |
|--|---|--|
| Density 0.322 lb/in ³ 8.90 g/cm ³ | Magnetic Permeability Ferromagnetic Saturation Magnetization App. 6 400 Gauss | Specific Heat 0.109 Btu/lb-°F 456 J/kg-°K |
| Specific Gravity 8.90 | Melting Range °F = 2615-2635 °C = 1435-1446 | |



ALLOY 200 / 201

THERMAL PROPERTIES //////////////////////////////////////

| Temperature | | Specific Heat | | Thermal Conductivity | | | | Electrical Resistivity | | Modulus of Elasticity | | Coefficient of Thermal Expansion | |
|-------------|------|---------------|-----------|----------------------|-------------------------------|-----------|-------------------------------|------------------------|---------------|-----------------------|---------------------|----------------------------------|----------------------|
| °C | °F | J/kg K | Btu/lb °F | Alloy 200 | | Alloy 201 | | μΩ cm | Ω circ mil/ft | kN/mm ² | 10 ³ ksi | 10 ⁻⁶ /K | 10 ⁻⁶ /°F |
| | | | | W/m K | Btu in.μ/ft ² h °F | W/m K | Btu in.μ/ft ² h °F | | | | | | |
| -200 | -328 | 150 | - | 78.5 | - | 93 | - | 2 | - | - | - | 10.1 | - |
| -184 | -300 | - | 0.045 | - | 540 | - | 640 | - | 15 | - | - | - | 5.8 |
| -129 | -200 | - | 0.076 | - | 530 | - | 630 | - | 21 | - | - | - | 6.8 |
| -100 | -148 | 355 | - | 75 | - | 87 | - | 4.5 | - | - | - | 11.3 | - |
| -73 | -100 | - | 0.091 | - | 505 | - | 590 | - | 33 | - | - | - | 6.3 |
| 0 | 32 | 426 | 0.102 | 71.5 | 500 | 81 | 560 | 8.5 | 51 | 207 | 30 | - | - |
| 20 | 68 | 456 | 0.109 | 70.5 | 490 | 79 | 550 | 9 | 54 | 205 | 29.7 | - | - |
| 93 | 200 | - | 0.113 | - | 465 | - | 510 | - | 75 | - | 29.1 | - | 7.4 |
| 100 | 212 | 475 | - | 66.5 | - | 73 | - | 13 | - | 200 | - | 13.3 | - |
| 200 | 392 | 500 | - | 61.5 | - | 67 | - | 19 | - | 196 | - | 13.9 | - |
| 204 | 400 | - | 0.132 | - | 425 | - | 460 | - | 114 | - | 28.4 | - | 7.7 |
| 300 | 572 | 570 | - | 57 | - | 60 | - | 26 | - | 190 | - | 14.3 | - |
| 316 | 600 | - | 0.139 | - | 390 | - | 410 | - | 162 | - | 27.3 | - | 8 |
| 400 | 752 | 530 | - | 56 | - | 57 | - | 33 | - | 182 | - | 14.8 | - |
| 427 | 800 | - | 0.124 | - | 390 | - | 390 | - | 207 | - | 26.1 | - | 8.3 |
| 500 | 932 | 525 | - | 57.5 | - | 58.5 | - | 37 | - | 175 | - | 15.2 | - |
| 538 | 1000 | - | 0.128 | - | 405 | - | 410 | - | 229 | - | 24.7 | - | 8.5 |
| 600 | 1112 | 535 | - | 60 | - | 61 | - | 40 | - | 165 | - | 15.6 | - |
| 649 | 1200 | - | 0.130 | - | 420 | - | 430 | - | 250 | - | 23.2 | - | 8.7 |
| 700 | 1292 | 550 | - | 62 | - | 63 | - | 43 | - | 153 | - | 15.8 | - |
| 760 | 1400 | - | 0.133 | - | 435 | - | 445 | - | 265 | - | 21 | - | 8.9 |
| 800 | 1472 | 565 | - | 64 | - | 65.5 | - | 45 | - | 140 | - | 16.2 | - |
| 871 | 1600 | - | 0.137 | - | 455 | - | 465 | - | 285 | - | 19.6 | - | 9.1 |
| 900 | 1652 | 580 | - | 66.5 | - | 68 | - | 48 | - | 134 | - | 16.5 | - |
| 982 | 1800 | - | 0.144 | - | 470 | - | 480 | - | 305 | - | - | - | 9.3 |
| 1000 | 1832 | 590 | - | 69 | - | 70.5 | - | 51 | - | - | - | 16.7 | - |



ALLOY 200/201

CORROSION RESISTANCE

Alloy 200 and Alloy 201 are used primarily in reducing or neutral environments. The alloys may also be used in oxidizing environments that cause the formation of a passive oxide film.

Examples of environments in which Alloy 200 and Alloy 201 have been used are caustics, high temperature halogens and salts other than oxidizing halides. They are also used in the food processing industry.

The nickel content of these alloys renders them virtually immune to chloride stress corrosion cracking. The alloys have been used in fresh and many other process waters with superior results.

Alloy 200 and Alloy 201 have been used in caustic solutions such as those encountered in the production of caustic soda when chlorate level is low. Nickel is not susceptible to caustic stress corrosion cracking. When chlorate is about 0.1 %, as in diaphragm cell technology used in caustic soda production, an iron chromium alloy might be preferred.

Sulfurous atmospheres are corrosive to nickel alloys, especially above 600 °F (316 °C). Oxidizing mineral acids and oxidizing salts are also corrosive.

AQUEOUS CORROSION DATA

| Test Environment | | Temperature | | Corrosion Rate |
|----------------------|---|-------------|-----|----------------|
| Name | Media & Concentration | °F | °C | mpy |
| Acetic Acid | 5 % CH ₃ CO ₂ H w/ air | 70 | 21 | 40 |
| Acetic Acid | 10 % CH ₃ CO ₂ H | 86 | 30 | 3.4 |
| Acetic Acid | 56 % CH ₃ CO ₂ H | 176 | 80 | 66 |
| Acetic Acid | 85 % CH ₃ CO ₂ H w/ air | 70 | 21 | 400 |
| Acetic Acid | 98 % CH ₃ CO ₂ H | 241 | 116 | 12 |
| Caustic Soda | 50 % NaOH | 195 | 90 | 0.55 |
| Caustic Soda | 50 % NaOH | 310 | 155 | 0.5 |
| Caustic Soda | 75 % NaOH | 250 | 120 | 1 |
| Formic Acid (liquid) | 90 % CH ₂ O ₂ | 70 | 21 | 4 |
| Formic Acid (vapor) | 90 % CH ₂ O ₂ | 70 | 21 | 7 |
| Hydrochloric Acid | 1 % HCl | 214 | 101 | 680 |
| Hydrochloric Acid | 10 % HCl | 86 | 30 | 80 |
| Hydrochloric Acid | 10 % HCl | 221 | 105 | 8000 |
| Nitric Acid | 10 % H ₃ PO ₄ | 216 | 102 | 12000 |
| Phosphoric Acid | 10 % H ₃ PO ₄ | 75 | 24 | 0.6 |
| Phosphoric Acid | 10 % H ₃ PO ₄ | 214 | 101 | 154 |
| Phosphoric Acid | 40 % H ₃ PO ₄ | 75 | 24 | 1 |
| Sodium Hypochlorite | 500 ppm NaClO | 77 | 25 | 0.8 |
| Sulfuric Acid | 2 % H ₂ SO ₄ | 70 | 21 | 2 |
| Sulfuric Acid | 5 % H ₂ SO ₄ | 140 | 60 | 10 |
| Sulfuric Acid | 5 % H ₂ SO ₄ w/ air | 86 | 30 | 61 |
| Sulfuric Acid | 19 % H ₂ SO ₄ | 223 | 106 | 110 |
| Sulfuric Acid | 20 % H ₂ SO ₄ | 70 | 21 | 4 |
| Sulfuric Acid | 50 % H ₂ SO ₄ w/ air | 86 | 30 | 16 |
| Sulfuric Acid | 50 % H ₂ SO ₄ | 255 | 124 | 1000 |
| Sulfuric Acid | 96 % H ₂ SO ₄ w/ air | 86 | 30 | 10 |



ALLOY 200 / 201

HEAT TREATMENT

Considerable latitude exists in heat treating temperatures for Alloy 200 and Alloy 201. Temperatures in the range of 1300 °F (704 °C) to 1700 °F (927 °C) may be employed. Car or box anneal cycles which employ long furnace times should use the lower temperatures. Continuous anneal cycles which employ short times should use higher temperatures. If heavy forming is required, anneal time may be increased to provide fully soft material.

Sulfur, phosphorus, lead, zinc and other low-melting metals are potential contaminants which must be avoided. Only clean materials should be exposed to heat treating operations.

Exposure of Alloy 200 and Alloy 201 to oxygen at heat treating temperatures results in formation of a surface oxide. Reducing atmospheres such as dry hydrogen are preferred to maintain a scale-free surface.

FORMABILITY

Alloy 200 and Alloy 201 can be formed by most common commercial fabrication practices. Annealed mechanical properties are similar to those of mild steel but forming operations work harden the material. Intermediate anneals should be considered for extensive cold forming.

COLD FORMING

Alloy 200 and Alloy 201 can be worked by all conventional cold-forming methods. In general, the alloys will behave similarly to mild steel with the exception that because of the higher elastic limit of these alloys, greater force will be required to perform the operations (with Alloy 201 requiring slightly less force due to its slightly lower range of mechanical properties). As such, manual operations such as spinning and hand hammering are limited to simple shapes. Severe work can be done manually only with the assistance of frequent anneals to restore softness.

HOT FORMING

Alloy 200 and Alloy 201 can be easily formed to practically any shape. Making sure that the material is at the optimum temperature during deformation is the most important factor in achieving hot malleability. The recommended temperature range for hot forming is 1200-2250 °F (650-1230 °C). Heavy forging should be done above 1600°F (870°C) as the metal stiffens rapidly below this temperature. Light forging below 1200°F (650°C) will produce higher mechanical properties. In any forming process, care should be exercised to avoid heating above the upper limit of 2250 °F (1230 °C).

MACHINING

Alloy 200 and Alloy 201 can be machined at common commercial rates. The material tends to flow under pressure of the tool cutting edge and form long stringy chips. To avoid a built-up edge, tools should be ground with very high positive rake angles (angles of 40°-45° have been used in some instances). High-speed or cast-ally tools should be used.

Chip action is substantially better with material in the harder tempers. Cold drawn bar in the as-drawn or stress-relieved condition will machine easier than material in the annealed condition.



ALLOY 200 / 201

WELDING

Alloy 200 and Alloy 201 can be joined by a wide variety of processes including inert gas welding processes, resistance welding, soldering and brazing. In all of these procedures, thorough cleaning of the joint area is necessary to avoid embrittlement from such sources as lubricants, paints and marking devices.

Welding procedures for Alloy 200 and Alloy 201 are similar to those used for austenitic stainless steels. Neither preheating, nor post-weld heat treatment are generally required. Joint design is similar to that used for austenitic stainless steels with two exceptions. The first is the need to accommodate the sluggish nature of the molten weld material, necessitating a joint design sufficiently open to allow full filler wire access to fill the joint. The second is the high thermal conductivity and purity of the material which makes weld penetration lower than in austenitic stainless steels.

A variety of stabilized nickel base fillers are available to join Alloy 200 or Alloy 201 sections. Other materials are available for joining Alloy 200 and Alloy 201 to dissimilar materials.

Special care should be taken in choosing filler metals to join Alloy 201. These materials should be low in carbon and stabilized to avoid the introduction of free carbon to Alloy 201 with the subsequent potential for embrittlement at higher operating temperatures.

